# Size optimization of truss structures employing flower pollination algorithm without grouping structural members

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*Abstract:* - In the optimum design of the cross-sectional areas of the structural members, swarm intelligence based methods are effective in finding optimum designs. In order to increase the level of the feasibility of the approaches, the members of the structures are grouped. In that case, the computational cost decreases, but the exact optimum design of the structure cannot be found. In that case, the employed methodology must be sufficiently fast if the members are not grouped. In this paper, the truss structural systems are investigated without grouping. The methodology employs the flower pollination algorithm and an iterative constraint handling strategy is applied for design constraints about compression, tension and displacement limits. The method is effective in finding truss structure designs with smaller cross-sectional areas than those of the existing strategy using grouping of structural members.

*Key-Words:* Truss structures, Flower Pollination Algorithm, Structural member without grouping, Size optimization, Optimization, Nature inspired swarm intelligence.

## **1** Introduction

Nature-inspired methods and metaheuristic algorithms are commonly used in the design of structural members in civil engineering. The main purpose of the design is to find the design with the minimum material cost which is directly related to the total weight of the structure. To ensure the design constraints with an economical design, the engineering problem becomes highly non-linear. In that case, the only way is to use numerical iterations. In order to find a member with precise solutions and good computational cost, the studies on this subject is very active in employing swarm intelligence based methods.

The most popular optimization problem is the size optimization of three-dimensional truss structures. For this type of problems, Adeli and Kamal used a dual simplex algorithm [1]. Genetic algorithm has been also employed in optimum design of truss structures [2-3]. Camp and Bichon investigated truss structures by using ant colony optimization [4]. The big bang-big crunch (BB-BC) algorithm was of metaheuristic another example methods employed for truss structure optimization [5]. Li et al. developed hybrid method containing particle swarm optimizer with passive congregation and harmony search for truss structures [6]. Particle swarm optimization was used in the methodology developed by Perez and Behdinan [7]. In the sizing and layout optimization of truss structures, simulated annealing was used by Lamberti [8]. Kaveh and Talatahari employed BB-BC hybridized with particle swarm optimization and suboptimization mechanism [9]. Sonmez combined artificial bee colony with adaptive penalty function for truss structure optimization [10]. Two variations of harmony search (efficient and self-adaptive) were used by Degertekin in truss system optimization [11]. Teaching learning based optimization (TLBO) was employed by Camp and Farshchin in the optimum design of truss structures [12]. Hybrid particle swallow swarm optimization was employed by Kaveh et al. for truss structure [13]. Kaveh et al. employed chaotic swarming of particles in size optimization of truss systems [14]. Colliding bodies optimization (CBO) was also employed for truss system optimization [15]. The enhanced version of CBO was used by Kaveh and Ilchi Ghazaan for the same types of problem [16]. Flower pollination algorithm (FPA) developed by Yang [17] was also used by Bekdas et al. for sizing optimization of truss structures [18].

In the documented methods, the members of the truss structures are grouped and the members of different design variables are reduced. In that case, the optimization time is reduced, but the precise optimum results cannot be found. The FPA is effective in saving computation times and this algorithm can be also used if the members are not grouped. Another issue in grouping of members is how we group these members and if these groups are the best or not. For these reasons, the members are not grouped in this study. FPA is employed and the methodology is summarized in the second section. The detailed information and formulations about the method can be found in [17] including a good design constraint handling strategy.

## 2 The Design Methodology

The inspiration of FPA is the flow pollination process of flowering plants. Yang [17] developed FPA by using the four rules about biotic (cross) pollination, abiotic (self) pollination, flower constancy and a switch probability. The design methodology of the truss sizing optimization problem employing FPA can be explained in three steps.

As all structural optimization problems, the design constants, ranges of design variables and design constraints are defined in the first step. Also, the algorithm constraints of FPA such as flower number (n), switch probability (p) and maximum generation number ( $g_{max}$ ) are entered.

In the second step, the initial values of design variables are randomly assigned before the iterative process. For all sets of design variables, structural analyses are done in order to control the design constraints. An iterative constraint handling strategy defined in [18] is applied.

As a metaheuristic algorithm, the design variables are updated in two ways and a switch probability controls the type of modification. In global search, biotic pollination is imitated. In that pollination, pollinators carry the pollens and they obey Lévy flight rules. For that reason, a new design variables  $(X_i^{t+1})$  are calculated according to previous solution  $(X_i^{t})$ , Lévy distribution (L) and the best design variables with the maximum weight (g<sup>\*</sup>) as seen Eq. (1).

$$x_i^{t+1} = x_i^t + L(x_i^t - g_*)$$
 (1)

In local optimization, abiotic pollinators is used. In that type of pollination, the pollinator is the different flowers of the same plant. As seen in Eq. (2),  $X_i^{t+1}$  is generated according to  $\in$  ( a random number between 0 and 1) and the variables of  $j^{th}(X_j^t)$  and  $k^{th}(X_k^t)$  flowers which are randomly chosen.

$$x_i^{t+1} = x_i^t + \epsilon (x_j^t - x_k^t)$$
 (2)

The iterative process is carried out for maximum number of generations and the weight minimization is done as optimization objective.

## **3** Numerical Example

As numerical examples, 25 bar and 72 bar 3D truss structures are optimized without grouping design variables. The analyses are carried out by taking n=20, p=0.5 and  $g_{max}$ =100000, respectively as done in [18].

#### 3.1 25 bar truss structure

The model of 25 bar structure is shown in Fig. 1 and loading cases are given in Table 1. In this example,

the elasticity modulus and density are taken as 10 Msi and 0.1 lb/in<sup>3</sup>. The ranges of cross sectional areas (design variables) are between 0.01 and 3.4 in<sup>2</sup>. The compression and tension constraints are different for different members and these limits are shown in Table 2. The optimum results are given in Table 3. The best weight is 543.20 lb. This value is 545.159 lb if the members of truss are grouped [18].

#### 3.2 72 bar truss structure

The FPA is effective to solve 72 bar truss structure (Fig. 2) optimization problem without grouping

design variables. The loading case of 72 bar truss structure is shown in Table 4. The material properties are the same as the first example. The maximum displacement limits is  $\pm 0.25$  in for all nodes and stress limits  $\pm 25$  ksi for tension and compression of all members. The cross sectional areas are randomized between 0.1 and 3.0 in<sup>2</sup>. The optimum results are presented in Table 5 and the optimum weight is 60.5180 lb. If the design variables are grouped, the optimum value is 379.534 lb [18].

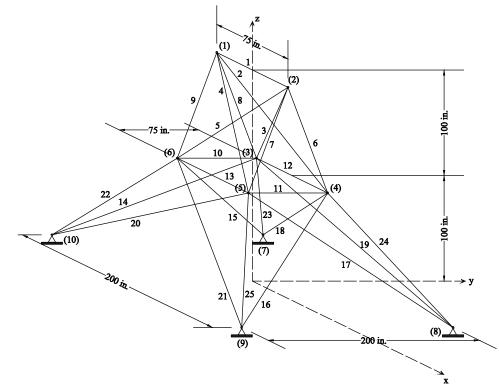


Figure 1 25-bar truss structure.

|                                                             |      | THE LUADING CASES OF 2. |                       |                       |
|-------------------------------------------------------------|------|-------------------------|-----------------------|-----------------------|
| Case                                                        | Node | P <sub>x</sub> (kips)   | P <sub>v</sub> (kips) | P <sub>z</sub> (kips) |
|                                                             | 1    | 1.0                     | 10.0                  | -5.0                  |
|                                                             | 2    | 0.0                     | 10.0                  | -5.0                  |
| 1                                                           | 3    | 0.5                     | 0.0                   | 0.0                   |
|                                                             | 6    | 0.0                     | 0.0                   | 0.0                   |
| 2                                                           | 1    | 0.0                     | 20.0                  | -5.0                  |
| 2                                                           | 2    | 0.0                     | -20.0                 | -5.0                  |
|                                                             |      |                         |                       |                       |
| TABLE II. The design constraint limits of 25-bar structure. |      |                         |                       | RE.                   |

|         | TABLE II. THE DESIGN CONSTRAINT EIMITS OF 25-BAR STRUCTURE. |               |  |  |
|---------|-------------------------------------------------------------|---------------|--|--|
| Members | Compression (ksi)                                           | Tension (ksi) |  |  |
| 1       | 35.092                                                      | 35            |  |  |
| 2-5     | 11.590                                                      | 35            |  |  |
| 6-9     | 17.305                                                      | 35            |  |  |
| 10,11   | 35.092                                                      | 35            |  |  |
| 12,13   | 35.092                                                      | 35            |  |  |
| 14-17   | 6.759                                                       | 35            |  |  |
| 18-21   | 6.959                                                       | 35            |  |  |
| 22-25   | 11.082                                                      | 35            |  |  |
|         |                                                             |               |  |  |

| Member           | Area (in <sup>2</sup> ) | Member | Area (in <sup>2</sup> ) | Member | Area (in <sup>2</sup> ) |
|------------------|-------------------------|--------|-------------------------|--------|-------------------------|
| No               |                         | No     |                         | No     |                         |
| 1                | 0.0100                  | 11     | 0.0104                  | 21     | 1.3793                  |
| 2                | 2.3903                  | 12     | 0.0100                  | 22     | 2.3446                  |
| 3                | 1.8524                  | 13     | 0.0100                  | 23     | 2.5744                  |
| 4                | 2.0935                  | 14     | 0.7058                  | 24     | 3.1464                  |
| 5                | 1.9749                  | 15     | 0.5950                  | 25     | 2.5920                  |
| 6                | 2.9549                  | 16     | 0.8043                  |        |                         |
| 7                | 2.9379                  | 17     | 0.6149                  |        |                         |
| 8                | 3.0085                  | 18     | 1.7011                  |        |                         |
| 9                | 2.4974                  | 19     | 1.7259                  |        |                         |
| 10               | 0.0100                  | 20     | 1.8375                  |        |                         |
| Best Weight (lb) |                         | 543.20 |                         |        |                         |

| 11122111, $11120111000100200120012000000000000000$ | TABLE III. | THE OPTIMUM RESULTS OF 25-BAR STRUCTURE |
|----------------------------------------------------|------------|-----------------------------------------|
|----------------------------------------------------|------------|-----------------------------------------|

TABLE IV.The loading cases of 72-bar structure

| Node  | Px     | Ру                   | Pz                               |
|-------|--------|----------------------|----------------------------------|
|       | (kips) | (kips)               | (kips)                           |
| 17-20 | -5.0   | -5.0                 | -5.0                             |
| 17    | 5.0    | 5.0                  | -5.0                             |
|       |        | (kips)<br>17-20 -5.0 | (kips) (kips)<br>17-20 -5.0 -5.0 |

TABLE V. THE OPTIMUM RESULTS OF 72-BAR STRUCTURE.

| Member No           | Area (in <sup>2</sup> ) | Member No | Area (in <sup>2</sup> ) | Member No | Area (in <sup>2</sup> ) |
|---------------------|-------------------------|-----------|-------------------------|-----------|-------------------------|
| 1                   | 2.3656                  | 25        | 0.4861                  | 49        | 0.1125                  |
| 2                   | 0.5654                  | 26        | 0.7112                  | 50        | 0.2167                  |
| 3                   | 2.9571                  | 27        | 0.7178                  | 51        | 0.1000                  |
| 4                   | 0.1570                  | 28        | 0.4372                  | 52        | 0.3199                  |
| 5                   | 0.4829                  | 29        | 0.4478                  | 53        | 0.1936                  |
| 6                   | 0.1626                  | 30        | 0.2355                  | 54        | 0.1000                  |
| 7                   | 0.8478                  | 31        | 0.1018                  | 55        | 0.5265                  |
| 8                   | 0.2821                  | 32        | 0.1415                  | 56        | 0.8380                  |
| 9                   | 0.8694                  | 33        | 0.1263                  | 57        | 0.8082                  |
| 10                  | 0.5814                  | 34        | 0.1031                  | 58        | 0.3976                  |
| 11                  | 0.1918                  | 35        | 0.1018                  | 59        | 0.1530                  |
| 12                  | 0.5212                  | 36        | 0.1606                  | 60        | 1.2308                  |
| 13                  | 0.1004                  | 37        | 0.2796                  | 61        | 0.6596                  |
| 14                  | 0.1000                  | 38        | 0.9654                  | 62        | 0.2411                  |
| 15                  | 0.1393                  | 39        | 2.1531                  | 63        | 0.1087                  |
| 16                  | 0.1225                  | 40        | 0.5820                  | 64        | 0.5861                  |
| 17                  | 0.1679                  | 41        | 0.5124                  | 65        | 1.0083                  |
| 18                  | 0.1000                  | 42        | 0.1039                  | 66        | 0.1378                  |
| 19                  | 1.5037                  | 43        | 0.5328                  | 67        | 0.2458                  |
| 20                  | 0.1000                  | 44        | 0.4544                  | 68        | 0.1202                  |
| 21                  | 2.5814                  | 45        | 0.6972                  | 69        | 0.1040                  |
| 22                  | 0.2401                  | 46        | 0.6018                  | 70        | 0.1233                  |
| 23                  | 0.2092                  | 47        | 0.2437                  | 71        | 0.5579                  |
| 24                  | 0.4181                  | 48        | 0.4370                  | 72        | 0.1296                  |
| Best Weight (lb) 36 | 50.5180                 |           |                         |           |                         |

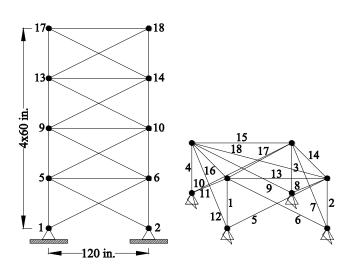


Figure 2 72-bar truss structure.

### 4 Conclusions

As a conclusion, FPA is also effective if the members of truss structures are not grouped. In that case, precise optimum results can be found. The results of the optimization problems are updated by 3.6% and 5% for the first and second examples. Future studies will focus on the extension of the current method and results to more complicated real-world design applications.

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