

Fig. 8. System frequency dynamic response during system frequency disturbance considering three different power imbalances (ΔP_L), $H_{syn} = 0.25H_{WTG}$.

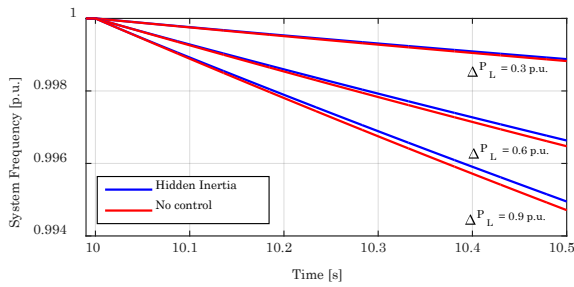


Fig. 9. Details at the very beginning (0.50 sec) of the system frequency response.

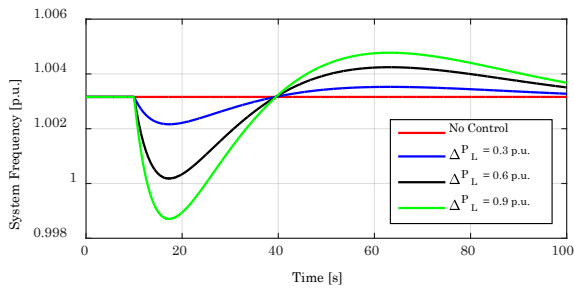


Fig. 10. Rotor speed response during system frequency disturbance. Inertia controller gain adjusted at $H_{syn} = 28.0$ sec.

It should be noticed, the implementation of this kind of frequency support strategy has to be properly designed since as high value of the synthetic inertia may lead to a problem in the wind turbine dynamic. In Fig. 10 and 11 show the system frequency response and generator rotor speed in case of inertial controller gain adjusted to three times the wind generator inertia ($H_{syn} = 3H_{WTG}$) and system frequency disturbance of 0.90 pu

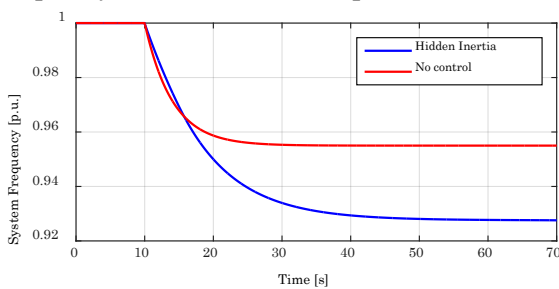


Fig. 11. System frequency response: System frequency disturbance $\Delta P_L = 0.90$ pu and inertia controller gain $H_{syn} = 3H_{WTG}$.

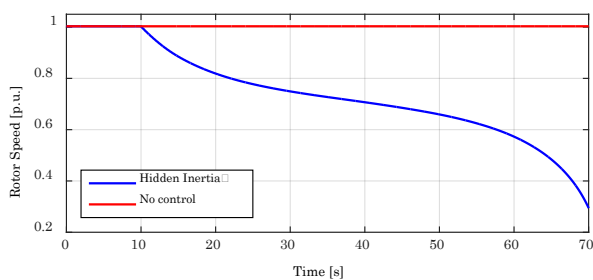


Fig. 12. Rotor speed response: $\Delta P_L = 0.90$ pu and inertia controller gain $H_{syn} = 3H_{WTG}$.

Fig. 12 shows a clear condition where the wind turbine generator stalls by means of a drift of the rotor speed and the consequent shut down of the WTG. This is a very critical condition for frequency stability since it produces a further system frequency disturbance by losing wind turbine generation and decreasing in frequency. Analysing the mathematical rule of the synthetic inertia controller (5), it is possible to notice that its contribution does not provide a change in the possible steady-state equilibrium point of the power system, since the additional term is proportional to the time derivative of frequency. This suggests that the frequency instability problem is not related to the feasibility of the system equilibrium point but is probably related to the interaction between the WTG controller and the synthetic inertia one.

The limit value of the synthetic inertia controller gains for the stable operation of the system vary in accordance with the amplitude of the frequency disturbance. In this paper, the limit values of stable conditions are obtained by means of dedicated simulations, Table 1 shows the results for the three-power imbalance conditions used in the previous simulations.

Table 1: Hidden Inertia limits for stable operation.

Load variation ΔP_L (pu)	Synthetic inertia limit $H_{syn,max}$ (sec)
0.30	$5H_{WTG}$
0.60	$3H_{WTG}$
0.90	$2H_{WTG}$

6 Conclusion

The aim of the present paper is to evaluate the inertial frequency support provided by variable speed wind generators. With this purpose, the main control strategy used to emulate an inertial behaviour of under converter generators where detailed, namely hidden inertia controller. It allows a fast active power contribution, fast power reserve emulation controller, that provides a smoother response depending on the slope included in the controller (P_{syn}/H_{syn}) and finally the droop control concept, that provides a contribution in a longer time frame similar to those provided by frequency control system for traditional power plants. The effect of this family of the control system has been evaluated considering the hidden inertia controller in a simplified wind turbine and network model implemented in Matlab/Simulink. The simulation highlighted the positive impact of the proposed controller on the system frequency in different load

conditions highlighting the positive contribution of Hidden Inertia Controller under different load variation conditions. In this sensitivity analysis, it was also possible to point out that high values of the synthetic inertia parameter, may destabilize the power system causing the stall of the WTG. Future works will concern the possibility to study the nature of this unstable behaviour of the Hidden Inertia controller in order to provide some criteria for the optimal and secure design of this controller. Moreover, it will be necessary to evaluate the possible integration of the synthetic inertial controller and the droop ones in order to achieve a more effective effect of a wind generator in the support of frequency beyond the first instants of the transient.

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