Performance Analysis of a Novel Architecture of Cs₂AgBiBr₆-based Tandem perovskite photovoltaics

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Abstract: Organic-inorganic hybrid perovskites can be used in solar cells with a single junction to achieve more than 25.5% efficiency. Optimizing the absorber layer (perovskite film) or investigating cutting-edge device designs, such as tandem-based solar cells that combine perovskite and silicon, can improve the device's power conversion efficiency (PCE). The overall power conversion efficiency (PCE) of a combination of silicon and perovskite solar cells can be increased above the Shockley-Queisser limit, which is the theoretical efficiency limit for single-junction solar cells. Utilizing a wider spectrum of solar light allows for this. This work shows how to model and optimize a stand-alone Cs₂AgBiBr₆ perovskite solar cell. Then, using SCAPS-1D, it merges that model with a crystalline silicon (c-Si) solar cell to simulate a tandem assembly. The goal of the project was to place a perovskite solar cell on top of a high-efficiency c-Si solar cell with a four-terminal (4T) structure to increase its efficiency. The simulation yielded an output voltage of 1.5V and a short-circuit current density of 23.07 MA/cm² for the Cs₂AgBiBr₆ perovskite solar cell, which translated into a power conversion efficiency of **29.66%.** The tandem arrangement exhibited a significantly higher power conversion efficiency (**43.76%**) than individual cells. The findings indicate that the Cs₂AgBiBr₆ perovskite solar cell can be used in tandem systems with c-Si solar cells to obtain very high levels of efficiency. This work offers significant new insights into the design of effective perovskite e-Si tandem solar cells

Keywords: Filtered Spectrum, Perovskite, SCAPS-1D, Tandem, Solar cell

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1. Introduction:

In an attempt to improve solar cell efficiency, multijunction cells—also referred to as tandem cells that are made up of solar cells with different band gaps are being investigated. Researchers want to exceed the Shockley-Queisser model's 31% power conversion efficiency (PCE) limit for singlejunction devices. As the world's energy demand is expected to rise from 15 TW in 2011 to an estimated 30 TW by 2050, this strategy is considered essential [1]–[3].

Tandem systems benefit from top absorber materials with a wide bandgap (WBG) and bottom absorbers with a narrow bandgap (NBG). With silicon (Si) serving as the bottom absorber and III-V compound semiconductor-based materials serving as the top absorber, current generation multi-junction tandem solar cells (MJ-TSCs) have reached a notable 39% conversion efficiency under 1 sun conditions [4]. However, the high cost and precise production requirements associated with III-V compounds pose barriers to their widespread commercial adoption [5].

The advent of perovskite materials has had an impact on the research landscape focusing on III-V materials over the past ten years. Benefits of perovskites include higher absorption coefficient, affordability, ease of production, longer carrier diffusion length, reduced carrier effective mass, and bandgap tunability. Perovskite materials are therefore thought to be possible replacements.

In an effort to lower the levelized cost of electricity (LCOE) and increase conversion efficiency in solar cell technology, two-junction tandem solar cells (2-

T TSCs) are being studied by researchers. With a PCE of 13.7%, Mailoa et al. (2015) made history by creating the first two-terminal (2-T) perovskite/Si TSC. Zheng et al. made further improvements by using SnO_2 as the interconnecting layer (ICL) and electron transport layer (ETL) of the top cell. This led to a PCE increase of 17.10% on a 16 cm2 tandem solar cell (TSC) [8].

Though halide double perovskites, or elpasolites, have been known to science for almost a century, the photovoltaic community has recently been more interested in them [9]. The double perovskite structure of these compounds is typified by the alternating octahedra BX6 and B'X6, which share a corner. This structure's arrangement of two distinct cations, B and B', creates a three-dimensional superstructure known as rock-salt ordering [10]. The overall charge of the combined B and B' cations must be +4 in order to preserve charge neutrality. This criterion opens up new options within the halide double perovskite family by making it easier to explore combinations combining 1+/3+ cations.

Two main factors are driving research on A2BB'X6 perovskites in the photovoltaics industry. In the first, the goal is to maintain the advantageous 3D network that is made up of inorganic corner-sharing octahedra. Concurrently, there is a desire to investigate Pb replacement with less hazardous materials. The goal of this method is to preserve the special qualities of 3D APbX₃ materials, such as their strong light absorption, low band gap (\approx 1.6 eV), extended lifetime of photogenerated electrons and holes, and evenly distributed carrier effective masses. Further increasing the adaptability of these materials is the ability to expand the spectrum of atoms that can be added to the B sites by utilizing double perovskites [11]

2. Device Structure

In the assessment of tandem solar cell performance, a common practice involves the separate simulation of the top and bottom sub-cells. In this modelling approach, the tunnel junction is assumed to be free of imperfections, and both optical and electrical losses at the interfaces are disregarded, as outlined in the standard multi-junction modelling model [12]–[15]. Tandem solar cell systems often feature perovskite solar cells as the top cell and silicon solar cells as the bottom cell.

The Cs₂AgBiBr₆ perovskite solar cell used in this experiment has a band gap of 1.64 eV and a thickness of 1.08 μ m, which together produce a high absorption coefficient and open-circuit voltage (Voc). A hole-transport layer (HTL) and an electrontransport layer (ETL) surround the perovskite layer. The HTL is made of NiO with a band gap of 3.7 and a thickness of 2 μ m. It has remarkable holetransport and stability characteristics. With a band gap of 3.6 and a thickness of 0.030 μ m, the SnO₂ used to make the ETL has a low bandgap and strong electron mobility.

Crystalline silicon (c-Si) cells, which have a high open-circuit voltage, low resistance, and long-term stability, make up the bottom cell. The bandgap and voltage of the c-Si cell are carefully adjusted to match those of the perovskite cell in order to maximize energy capture. Utilizing the high absorption coefficient of the perovskite cell, the high open-circuit voltage and low resistance of the c-Si cell, the advantageous features of the ETL (low bandgap and high electron mobility), and the effective hole-transport characteristics of the HTL, this tandem configuration turns out to be a very effective photovoltaic device. The structure of nonlead PSC is depicted in Fig 1.



Fig 1: Design of the non-lead PSC

Parameters	FTO	TiO ₂	Cs2AgBiBr6	NiO
Thickness (um)	0.05	0.1	0.6	0.1
Eg(eV)	3.6	3.26	1.72	3.8
χ (eV)	4.0	4.2	4.19	1.46
ϵ_r	9.0	10.0	5.8	10.7
Nc (cm ⁻³)	2.2x10 ¹⁸	2x10 ¹⁷	1x10 ¹⁶	2.8x10 ¹⁹
Nv (cm ⁻³)	1.8x10 ¹⁹	6x10 ¹⁷	1x10 ¹⁶	1x10 ¹⁹
$\mu_{\rm n}$ (cm ² /Vs)	100	100	11.81	12
$\mu_{\rm p}$ (cm ² /Vs)	25	25	0.49	2.8
Nd (cm ⁻³)	1x10 ¹⁸	1x10 ¹⁷	-	-
Na (cm ⁻³)	-	-	1x10 ¹⁸	1x10 ¹⁹

Table I: Reference Perovskite Solar Cell Input Parameters

Table I contains a list of the input values for the top cell, which were taken from the reference [31]. Now to get the best ETL and HTL materials such that the cell functioning is maximized, various ETL materials such as (AZO, SnO₂, CdS, IGZO, PCBM)

whose parameters are got from various published reports [17], [20]–[23] which are summarized in Table II are substituted and the simulation is carried out following the same method

Parameters	CdS	IGZO	SnO ₂	РСВМ	AZO
E _g (eV)	2.4	3.05	3.30	2	3.3
χ (eV)	4.2	4.16	4	3.9	3.8
ϵ_r	10	10	9	3.9	9
Nc (cm ⁻³)	2.2×10^{18}	5x10 ¹⁸	2.2x10 ¹⁷	2.5 x10 ²¹	4 x10 ¹⁸
Nv (cm-3)	1.8x10 ¹⁹	5x10 ¹⁸	2.2x10 ¹⁶	$2.5 \text{ x} 10^{21}$	1x10 ¹⁹
$\mu_{\rm n}$ (cm ² /Vs)	100	15	200	0.2	100
$\mu_{\rm p}$ (cm ² /Vs)	25	0.1	80	0.2	25
Nd (cm ⁻³)	1x10 ¹⁷	1x10 ¹⁸	1x10 ¹⁷	2.93 x10 ¹⁷	1x10 ¹⁸
Na (cm ⁻³)	0	0	0	0	0
Nt (cm ⁻³)	1x10 ¹⁷	1x10 ¹⁵	1x10 ¹⁵	1x10 ¹⁵	1x10 ¹⁵

Table II Properties of different E I L materials	Table	II	Properties	of	different	ETL	materials
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Various HTL materials such as $(Cu_2O, CuI, PEDOT: PSS, CuSbS_2, NiO, and CuSCN)$ whose parameters are also got from various published

reports [16]–[20] which are summarized in Table III are substituted and the simulation is done in the same method.

Parameters	Cu ₂ O	CuI	CuSCN	NiO	CuSbS ₂
E _g (eV)	2.17	2.98	3.4	3.8	1.58
χ (eV)	3.2	2.1	1.9	1.46	4.2
ϵ_r	6.6	6.5	10	11.7	14.6
Nc (cm ⁻³)	2.5x10 ²⁰	2.8x10 ¹⁹	$1.7 \mathrm{x} 10^{19}$	2.5×10^{20}	2x10 ¹⁸
Nv (cm ⁻³)	2.5 x10 ²⁰	1x10 ¹⁹	2.5x10 ²¹	2.5×10^{20}	1x10 ¹⁹
μ _n (cm²/Vs)	80	0.00017	0.00015	2.8	49
μ _p (cm²/Vs)	80	0.0002	0.1	2.8	49
Nd (cm ⁻³)	0	0	0	0	0
Na (cm ⁻³)	1x10 ¹⁸	1x10 ¹⁸	1x10 ¹⁸	1x10 ¹⁸	1.38x10 ¹⁸
Nt (cm ⁻³)	1x10 ¹⁵	1x10 ¹⁵	1x10 ¹⁴	1x10 ¹⁵	1x10 ¹⁴

Table III: Properties of different HTL materials

3. Methodology

3.1 Numerical Methods

In recent times, simulation treatments for the optimization and evaluation of various parameters have attracted the majority of interest in solar research. Planar heterojunction OIP solar cells have been numerically simulated in the current study using SCAPS 1D. JV curve, power conversion efficiency, projected energy band gap, etc. are performance metrics that may be evaluated by using the continuity equation for solving Poisson's equation. The PCE, FF, Jsc, and Voc are also calculated using these curves.

$$\begin{split} \frac{\mathrm{d}}{\mathrm{d}z} & \left[-\varepsilon(z) \frac{\mathrm{d}\emptyset}{\mathrm{d}z} \right] = q[p(z) - n(z) + N_D^+(z) - N_A^-(z) + p_t(z) - n_t(z)] \\ & \frac{\mathrm{d}p_n}{\mathrm{d}t} = G_p - \frac{p_n - p_{n0}}{\tau_p} + p_n \mu_p \frac{\mathrm{d}\xi}{\mathrm{d}z} + \mu_p \xi \frac{\mathrm{d}p_n}{\mathrm{d}z} + D_p \frac{\mathrm{d}^2 p_n}{\mathrm{d}z^2} \\ & \frac{\mathrm{d}n_p}{\mathrm{d}t} = G_n - \frac{n_p - n_{p0}}{\tau_n} + n_p \mu_n \frac{\mathrm{d}\xi}{\mathrm{d}z} + \mu_n \xi \frac{\mathrm{d}n_p}{\mathrm{d}z} + D_n \frac{\mathrm{d}^2 n_p}{\mathrm{d}z^2} \end{split}$$

Furthermore, it is important to note that the solar cell solely absorbs photons with energy greater than the semiconductors' band gaps, resulting in the production of holes and electron pairs [25]. The shortest wavelength of photons with sufficient energy to produce carriers is determined by Eg. Hence, the cut-off wavelength is given by:

$$=\frac{1240}{E_a(\text{eV})}(\text{nm}) \qquad -(1)$$

At J=0 mAcm-2, The greatest voltage that a solar cell can generate, known as the open-circuit voltage (Voc), can be represented as follows:

$$V_{\rm oc} = \frac{kT}{q} \ln\left(\frac{J_{sc}}{J_0} + 1\right) \tag{2}$$

where Jo is the saturation point current density, temperature is given by T, q is the carrier charge, and k is the Boltzmann constant. The FF is given by:

$$FF = \frac{P_m}{V_{\rm oc} \cdot J_{\rm sc}}$$
(3)

Once more, Green [28] provides a precise calculation for determining the FF:

$$FF = \frac{v_{oc} - \ln(v_{oc} + 0.72)}{v_{oc} + 1}$$
 (4)

where $v_{oc} = \left(\frac{V_{oc}}{V_{th}}\right)$ is normalized V_{oc}

The theoretical FF was to be determined in ideal conditions in the current work, though. The largest FF values come from Equation 5, which ignores resistive losses [28]. Moreover, the maximum power point of a solar cell's power output to power input ratio is indicated as follows:

$$\eta = \frac{P_{\rm m}}{P_{\rm in} \cdot A} \qquad -(5)$$

where Pin denotes the radiation's intensity at the incidence and A denotes the area. Once more, when the voltage across a solar cell is zero, the shortcircuit current is equivalent to the electricity that is flowing through the cell. It is supplied by and depends on the solar spectrum being used.

$$J_{\rm sc} = q \int_{E_g}^{\infty} \frac{dN_{ph}}{dhv} d(hv) \qquad -(6)$$

The Varshni relationship [29]–[31] yields the Tbased bandgap at random temperature, T.

$$E_g(T) = E_g(0) - \frac{\propto T^2}{(T+\beta)^2} \qquad -(7)$$

where α and β are constants, the crucial parameter that determines the Jsc is electron mobility, while electron affinity depends on the material. By altering the material's qualities, it can be altered. Furthermore, the simulation results will be extracted using Eqs. 1-8.

4. Results and Discussion

A tandem device is characterized by a sequential arrangement of two-cell combinations, forming a tandem structure with two terminals. Consequently, the open-circuit voltage (Voc) of the tandem cell is the cumulative sum of its sub-cell voltages. It is noteworthy that the short-circuit current (Jsc) of the entire device is constrained by the lowest junction current among the sub-cells, thereby setting a limit on the overall short-circuit current of the tandem device [32]. The subsequent section will encompass simulations for both the complete tandem device and the individual cells.

The reference PSC is optimized in the next section by choosing suitable ETL and HTL materials, maximizing the thickness of the absorber layer, examining the impact of defect densities in the absorber layer, maximizing the thickness of particular ETL and HTL materials, and lastly examining the impact of the PSC's bandgap. Summary of a previously published article using $Cs_2AgBiBr_6$ as an absorber layer is shown in Table IV

Device Architecture	JSC (mA/cm ²)	VOC (V)	FF (%)	PCE (%)
ITO/CuNiO/Cs2AgBiBr6/C60/BCP/Ag[24]	3.19	1.01	69	2.23
FTO/TiO ₂ /Cs ₂ AgBiBr ₆ /Spiro- OMeTAD/MoO ₃ /Ag [25]	3.28	1.01	65	2.51
FTO/TiO ₂ /Cs ₂ AgBiBr ₆ /N719/Spiro- OMeTAD/Ag [26]	5.13	1.06	51	2.84
ITO/SnO ₂ /Cs ₂ AgBiBr ₆ /spiro-OMeTAD/Au [27]	11.4	0.92	60.93	6.37
FTO/TiO ₂ /Cs ₂ AgBiBr ₆ /Cu ₂ O/Au.[28]	11.45	1.50	42.14	7.25
ITO/SnO ₂ /Cs ₂ AgBiBr ₆ / P3HT/Au [29]	6.39	2.02	90	11.32
FTO/ZnO/Cs2AgBiBr6/NiO/Au.[30]	20.69	1.29	81.72	21.88
Ni/NiOx/Cs ₂ AgBiBr ₆ /TiO ₂ /FTO/Al [31] [reference]	21.46	1.33	88.53	25.38
FTO/SnO2/Cs2AgBiBr6/ NiO/Au [This Work]	23.07	1.5	88.43	29.66

Table IV: Device parameter comparison of Cs₂AgBiBr₆ - based PSC with earlier reported outcomes

4.1 Selection of HTL layer

The material layer of a solar cell called the hole transport layer (HTL) facilitates the transfer of positive charges, or holes, from the absorber layer to the electrical interface. The HTL can raise the overall efficiency of the solar cell by reducing the possibility of hole and electron recombination at the interface between the light-absorbing layer and the electrical contact. If holes and electrons recombine at this contact, the solar cell's efficiency will drop since the latter cannot contribute to the current generated by the former. The HTL provides a path for the holes to follow in order to reach the electrical contact, which helps to prevent this recombination and increase the efficiency of the solar cell. Table 2 shows the simulation results of different HTLs. The bar plot represents the various HTLs' efficiency as shown in Fig 2.

Table 2: Simulation results of various HTLs

	Cu ₂ O	CuI	CuSC	CuSbS	NiO
			Ν	2	
Voc	1.320	0.97	1.25	1.157	1.504
	8	1			
Jsc	23.07	23.0 7	23.074	23.76	23.07 4
FF	78.96	74.8 7	78.10	83.71	85.43
PC E	24.06	16.7 8	22.54	23.03	29.66



Fig 2: Efficiency of various HTL materials

4.2 Selection of ETL layer

The job of the electron transport layer is to transfer electrons created in the absorber layer when sunlight splits into electron-hole pairs and moves them to the front contact of the photovoltaic solar cell. Moreover, it prevents the holes from passing through the layer of absorber and coming in contact with the head contact. As a result, we looked at the efficiency, open-circuit voltage, and current density of several ETLs. Table 3 shows the simulation results of different ETLs. The bar plot presents the various HTLs' efficiency as shown in Fig 3.

Table 3: Simulation results of various ETLs

	PCBM	AZO	CdS	IGZO	SnO ₂
Voc	1.5208	0.9512	1.34	1.157	1.504
Jsc	23.06	24.07	22.12	23.76	23.07
FF	78.96	77.87	74.10	83.71	85.43
PCE	23.06	19.78	20.43	23.03	29.66



Fig 3: Efficiency of various ETL materials

The effect of various ETL materials on the quantum efficiency (QE) of the PSCs are shown in Fig. 3. AZO has the lowest PCE, and should not be utilized to construct lead-free PSCs, according to our simulation. SnO2 has the highest Jsc and PCE when compared to all the other ETLs in the table. Therefore considering SnO_2 as ETL helps in achieving higher efficiency.

4.3 Effect of Absorber Layer Thickness

The thickness of the AL is an important factor in determining PSC performance [33]. Because it absorbs incoming photons and produces charge carriers, the absorber layer (AL) in perovskite solar cells (PSCs) is important to solar cell performance. The durability and diffusion length of photogenerated carriers are directly impacted by the quality of the AL, which is determined by parameters including film shape [34, 35]. To absorb the most photons possible, the AL thickness must be carefully selected. If the thickness is too thick, the reverse saturation current may be reduced.



Fig 4: Impact of thickness variation

Fig 4 illustrates the impact of varying absorber thickness, ranging from 500 to 1100 nm, on PSC performance, while keeping all other input properties constant. Observations reveal а systematic decrease in Voc (from 1.5061 to 1.5 V) with increasing AL thickness, while the average AL thickness concurrently enhances Jsc (from 22.66 to 23.07). The efficiency exhibits a peak value of 29.66 at 1100 nm, accompanied by a decrease in fill factor (FF) from 89.28 to 85.43%. However, as the AL thickness increases, the recombination of charge carriers within the material intensifies, leading to a decline in efficiency [36]. Hence, an optimal thickness of 400 nm for Cs₂AgBiBr₆ is identified for achieving high efficiency [36].

4.4 Effect of Absorber Layer Bandgap

Fig 5 shows the effect of absorber layer bandgap on PSC's efficiency. By altering the energy gap of the deflecting parts, optical deflection can be regulated to create a highly efficient device [37]. The energy gap of AL in PSC devices, however, plays a significant role in the eye twitching. Cs₂AgBiBr₆'s thickness was set at 1100 nm, while all other parameters stayed the same. Because of the absorber level's 1.64 eV bandgap (Eg), this design can provide a maximum PCE of 29.66% and a maximum FF of 85.43%.



Fig 5: Effect of Absorber Layer Bandgap

4.5 Effect of Absorber Layer Defect Density

Defects in any perovskite material are inevitable and might take the form of point defects such gaps, vacancies, Schottky and Frenkel defects, etc. On numbers and surfaces, other flaws like reflections and grain boundaries can also be seen. The process of self-doping perovskite layers, which captures charge carriers and encourages nonradiative recombination, can also result in impurity defects [38]. Furthermore, high defect density impair PSC performance. From 10^{13} to 10^{17} cm-3, the AL fault density has been tuned and altered in order to fully comprehend its effect. Fig 6 illustrates the impact of absorbent layer defect density. Voc essentially stays unchanged. When the defect density rises from 10^{16} to 10^{17} , Jsc experiences a fall in absorber layer concentration from 22.11 to 12.30 mA/cm2. According to the graph, PCE drops from 29.66 to 3.07% and FF drops from 85.43 to 22.94%.



Fig 6: Effect of Absorber Layer Defect Density

4.6. The Absorber Layer's Electron Affinity's Impact

Fig 7 illustrates the impact of absorber layer's electron affinity. The amount of energy needed to change a neutral atom into a negative ion is known as a molecule's electron affinity. One key factor impacting performance is the electrical affinity of the perovskite material, which can have a significant impact on device performance [37]. We conduct 3.6 to 4.2 eV and various electron withdrawals of Cs₂AgBiBr₆ up to the device configuration in order to ascertain the impact of electron withdrawal on the PSC performance parameters. A rise in Voc may transpire gradually as result of elevated electron absorption. a Additionally, PCE increased from linearly 24.68 to 29.66%.



Fig 7: The Absorber Layer's Electron Affinity's Impact

4.7 Effect of ETL Thickness

The tool's performance is significantly influenced by the thickness of the ETL. Fig 8 shows the effect of ETL thickness. In addition to serving as channels for electron transmission from the AL, the ETL separates the electrode from the absorber layer [38]. ETL size can make it more difficult for charged ions (holes and electrons) to access the anode and cathode electrodes by increasing series resistance, which might result in recombination [39]. However, if ETL size is too reduced (below 50 nm) at electrode between a and absorber, To explore the effect of modifying the ETL size on the trap performane, which is too thin to provide efficient separation, we simulated the trap when varying the ETL size from 30 to 150 nm. The highest level of efficiency attained was 29.66.



Fig 8: Effect of ETL Thickness

4.8. Impact of HTL/Absorber Interface Defect Density

Interfacial faults, or charge recombination centers, are caused by structural mismatches between the two components or by the introduction of external stimuli in PSCs [40]. The impact of the method is also significant for third-generation solar cells (especially from the mouthpiece). Furthermore, non-radiative losses resulting from positive potential at heterojunctions between perovskite/charge extraction layers (HTL or ETL) and perovskite absorber defects cause Voc loss. The interaction between many PSC layers also affects device performance and long-term stability. When grid-assisted non-radiative reconnection is employed with an interface that has many defects/voids or grid conditions, voltage and current losses result. In order to comprehend the impact of defect density at the HTL/absorber layer interface, we adjust this number from 10^{10} to 10^{21} cm⁻³. The HTL/AL interface's fault density has minimal bearing on the PSC's performance. As the faults increase from 10¹⁰ to 10¹⁸ cm-3, a progressive decline in the performance coefficients is seen. Significant variations in the interfacial defect density (from 10¹⁸ to 10²¹ cm-3) had no effect on these values. Fig 9 shows the impact of HTL/Absorber interface defect density



Fig 9: Impact of HTL/Absorber Interface Defect Density

4.9. Impact of ETL/Absorber Interface Defect Density

Forward network failures have a greater impact on a PSC device's performance than surface network issues. This behavior can be explained by the perovskite material's larger absorption coefficient, which increases photon absorption close to the front contact and, as a result, creates more pairs of electron holes there. At this point, it is understood how charge carriers differ from network-assisted recombination. Consequently, we discover that issues with the frontal interface significantly affect the functionality of the gadget. Consequently, we must concentrate on debugging the front end. A number of mechanics, including ionic liquids [41], anti-relationship [42], graphene-based, juicy-based, and probe-based probes -based on the [43] - have been created for the passive process of inter-form defects. By contrast, there is a significant decrease in Jsc (24.20 to 22.99 mA/cm2), which is caused by the defect of increasing bio density (from 10^{16} to 10^{18} cm-3). The Jsc variation of the first four steps $(10^{10} \text{ to } 10^{18} \text{ cm}-3)$ associated with interface defect density variation is relatively insignificant. Furthermore, as the SnO₂/Cs₂AgBiBr₆ interface defect density increases, a progressive decline in FF and PCE is also seen; FF fell from 85.43 to 73.15% and PCE fell from 29.66 to 24.63% as shown in fig 10. Fig 10 illustrates the impact of ETL/Absorber interface defect density





4.10 Effect of Operating temperature on device performance

The current investigation's general operating temperature throughout simulation was 300 K. PSCs can, however, have their temperature altered during production, characterisation, and external usage. Season, height, latitude, and the time of day in a particular place all have an impact on the operating temperature. The performance of a PSC device is influenced by its operating temperature as shown in fig 11. The primary source of the PCE's reduction with rising temperature is a drop in the Voc. Voc is being observed to drop with increasing or decrease in temperature.



Fig 11: The way that operating temperature affects the functionality of a device

4.11 Simulation of Tandem Solar cell:

The lower-energy photons in the mechanically stacked tandem perovskite solar cell are captured by the c-Si bottom cell, while the higher-energy photons are captured by the perovskite top cell. The perovskite layer is a potential material for photovoltaics because of its high light absorption coefficient, quick charge carrier mobility, and inexpensive cost. In contrast, the c-Si bottom cell is a proven material that has been commercialized for a considerable amount of time in the solar sector.

The tandem perovskite solar cell can overcome some of the drawbacks of single-junction cells and reach high conversion efficiencies by combining these two elements in a mechanically stacked structure. The commercialization of mechanically stacked tandem perovskite solar cells is contingent upon the development of robust and scalable production procedures, as the stability and longterm performance of perovskite materials remain to be explored.

A simple method has been used to simulate the tandem cell using the SCAPS-1-D simulation software. We conducted our investigation using mechanically stacked two-terminal tandem cells, which are effectively two diodes connected in series. We also applied the current matching condition between the top and bottom cells [44]. Even in the scenario where the voltage is obtained by adding the voltages of individual cells, the cell with the lower Jsc dominates the current-limiting criterion of the overall tandem arrangement. To match the current, either Jsc variation or maximum power current density (JMP) variation is employed.

Table 4: Results of Simulations

Cell	Voc	Jsc	FF	PCE
			(%)	(%)
(Top Cell)	1.5	23.07	88.43	29.66
c-Si (Bottom Cell)	0.74	21.28	85.25	22.78
(Tandem)	1.48	14.94	89.05	43.76

We adjust the bottom cell's thickness to determine the current matching point. According to Table 4, we get an efficiency of **43.76%** in our simulation.

5.Conclusion:

This research studies non-lead PSCs with Cs₂AgBiBr₆ perovskite as the absorber layer using SCAPS modelling. First, the best materials for the ETL and HTL, which are SnO₂ and NiO, respectively, are determined. Subsequently, the effects of absorber layer thickness, absorber layer defect density, absorber layer band-gap, SnO2 thickness, and NiO thickness on PSC performance are investigated. The PSC configuration is glass substrate/FTO/SnO₂/Cs₂AgBiBr₆/NiO/Au. According to the models, the absorber layer should have an optimal defect density of 1×10^{13} cm-3. Any higher defect densities will cause a decrease in solar cell performance since more recombination sites will form. Using this PSC as the top cell and c-Si as the bottom cell, we have also simulated the tandem structure. The efficiency has increased from 29.66% in a single structure to 43.76% in tandem, as we have shown. The results of this study will contribute to the development of effective and nonlead PSCs, increasing the utilization of solar, wave, and wind energy as sustainable energy sources.

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